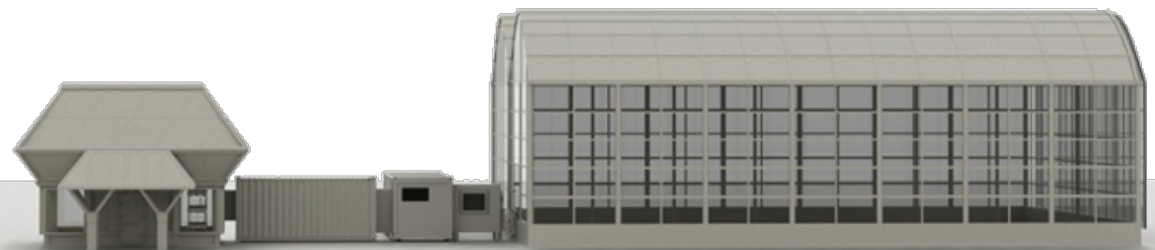




Assembly, Integration, and Initial Testing of the Carbon Dioxide Removal System at the Space Analog for the Moon & Mars

International Conference on Environmental Systems 2026
ICES-2026-524 | Rio Grande, Puerto Rico

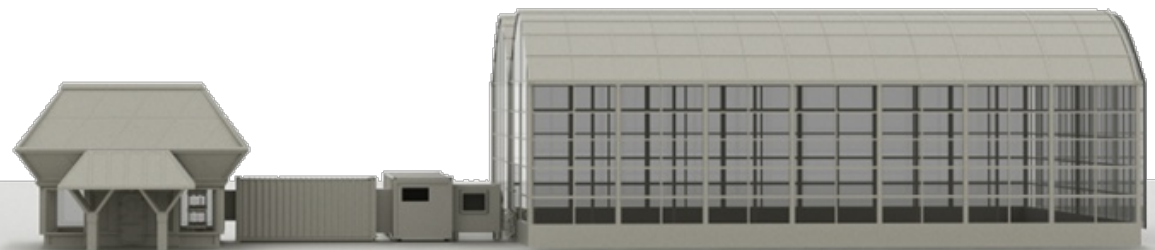
by Griffin Hentzen, Kai Staats, James Knox, Alyssa Ackerman, Jeffrey Buskirk, and Brendan Phoebe

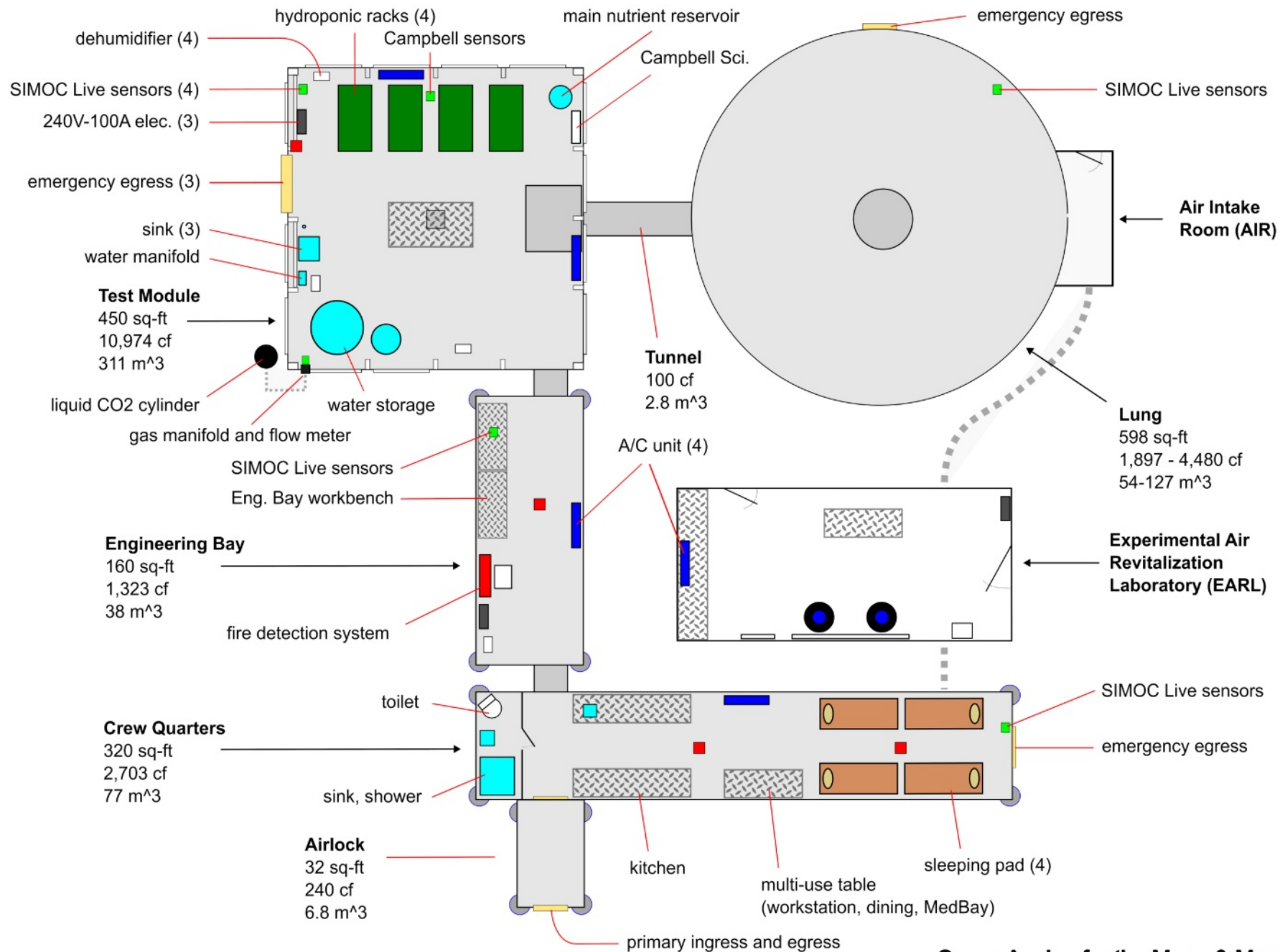


SAM Overview



- SAM: Space Analog for Moon & Mars
 - Hermetically sealed, pressurized (~0.05 psi over ambient) habitat research center located at the University of Arizona, Biosphere 2 campus
 - Modules
 - ☐ Variable volume pressure regulation module (“Lung”)
 - ☐ Controlled Environment (“Test Module”) with hydroponics for bioregeneration
 - ☐ Engineering Bay
 - ☐ Crew Quarters
 - ☐ Functional airlock
 - Primary research objectives
 - ☐ Studies in food cultivar bioregeneration and physicochemical air revitalization
 - ☐ Model validation with the SIMOC Live air quality monitor
 - ☐ Support of visiting “analog” teams



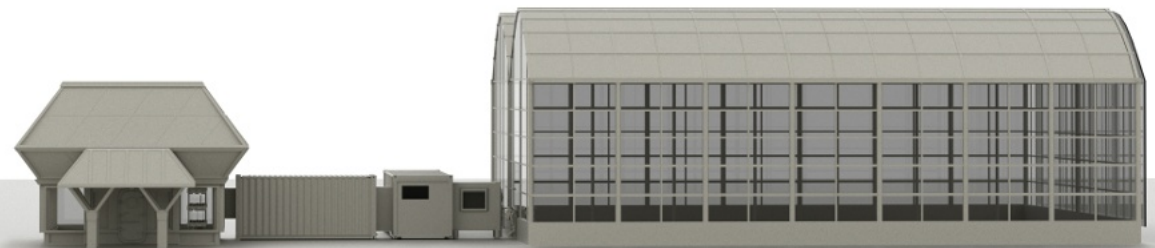




N1987B

Review of the prior, ICES 2025 paper

- Developed a mathematical model of the SAM habitat.
- Uses data from four prior, 4-person, 6-days missions at SAM.
- Took into account the general location of crew members while in SAM.
- Air circulation and ventilation to maintain desired CO₂ levels.
- Assumed constant temperature, perfect mixing, and ventilation at 24 SCFM.
- Predicted CO₂ scrubber efficiency as matching ISS 4BCO₂.
- Using the model, tested four ways in which to manage the air flow.



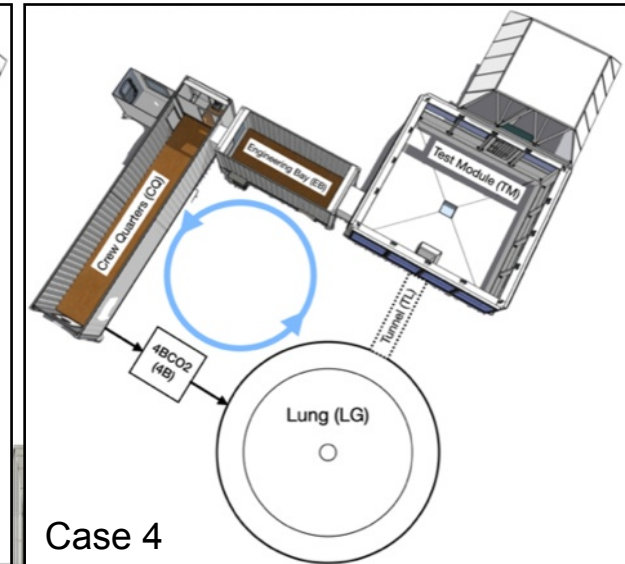
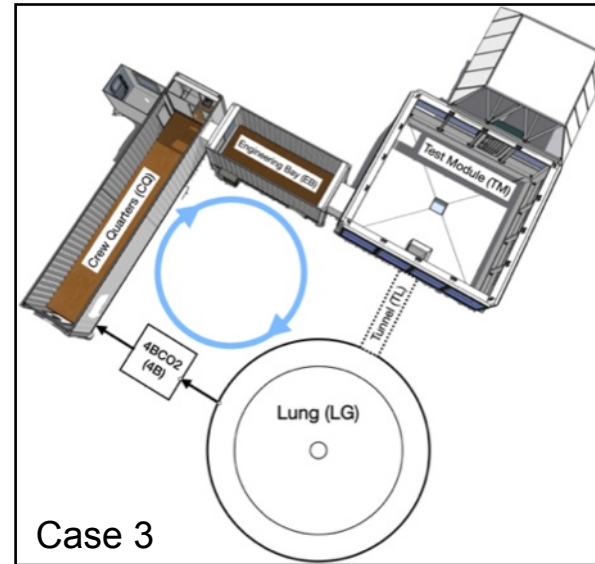
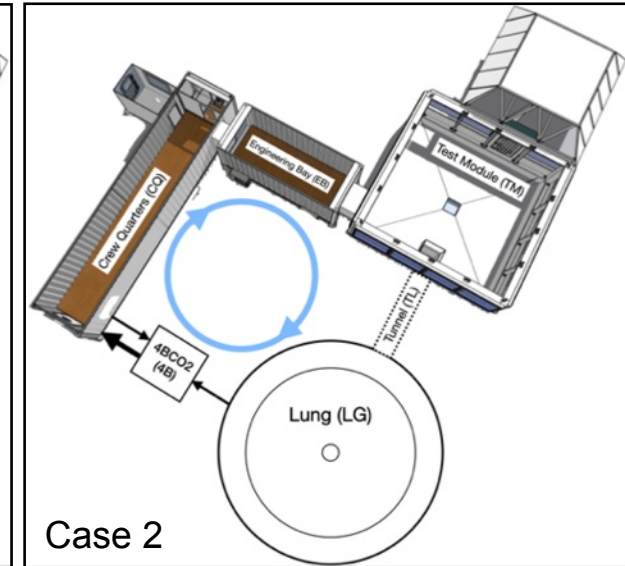
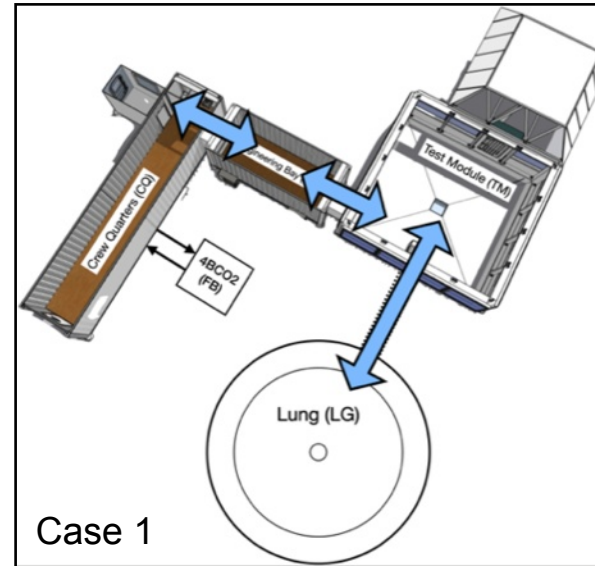
Analysis Cases

Summary of Conditions for Analysis Cases

	IMV Mode	IMV Direction	Scrubber Interface
Case 1	Interchange	N/A	Same Inlet/Outlet
Case 2	Racetrack	Clockwise	Same Inlet/Outlet
Case 3	Racetrack	Clockwise	Different In/Out
Case 4	Racetrack	Counter-Clockwise	Different In/Out

Assumptions/inputs

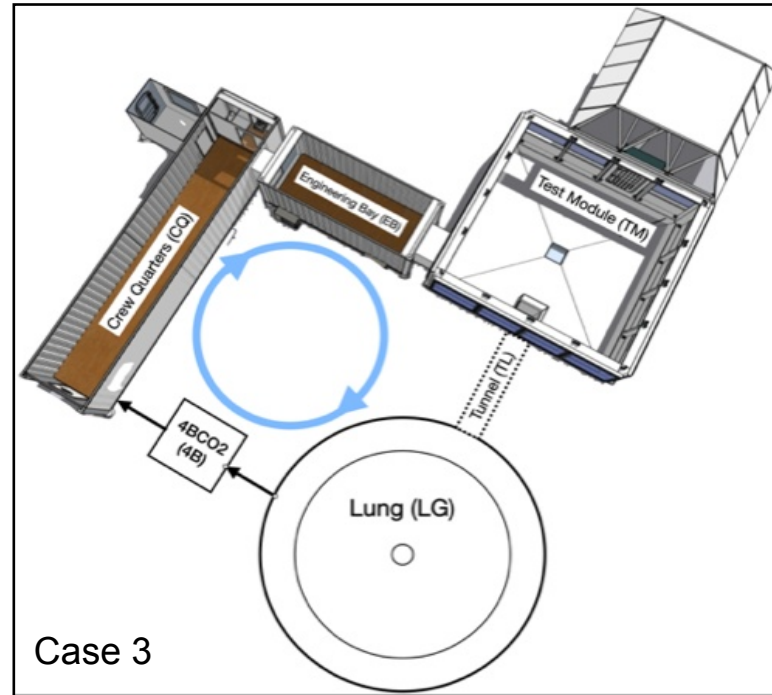
- Uniform IMV flow rate of 24 SCFM
- Scrubber flow rate of 24 SCFM
- No leakage out of modules (most conservative case)
- Crew metabolic and sleep rates set at average Human System Integration Requirements (HSIR) rates
- Crew locations/activities set by Imagination-1 mission
- CO₂ scrubber performance set by 4BCO₂ on ISS



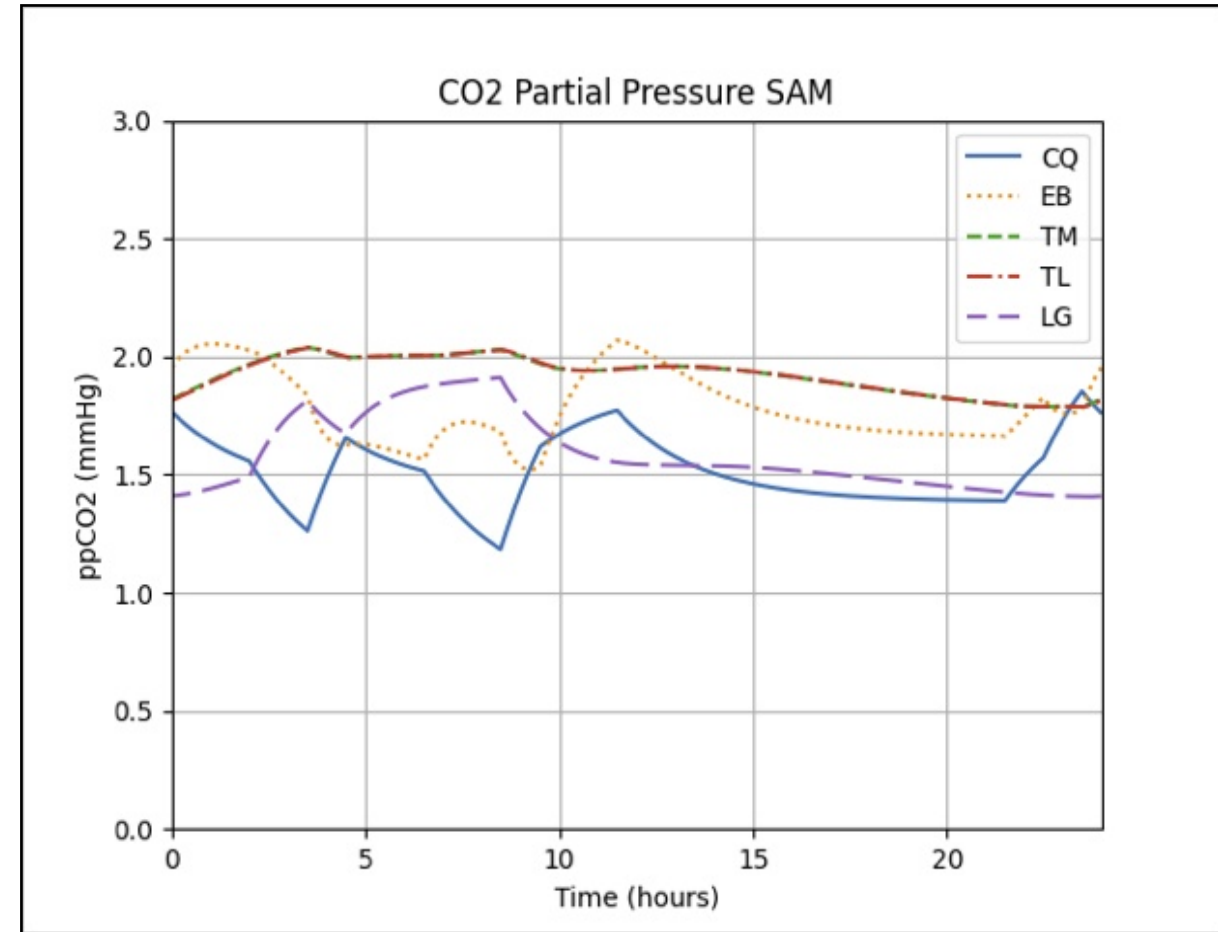
Analysis Case 3



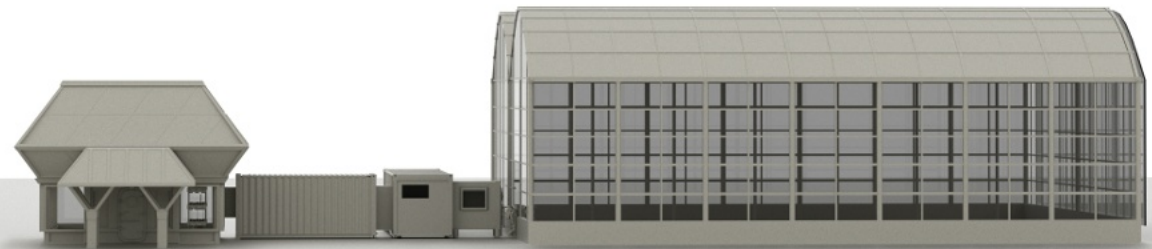
IMV Mode	IMV Direction	Scrubber Interface
Racetrack	Clockwise	Different In/Out



Case 3 Airflow



Case 3 Module CO₂ Simulation



Analysis Summary

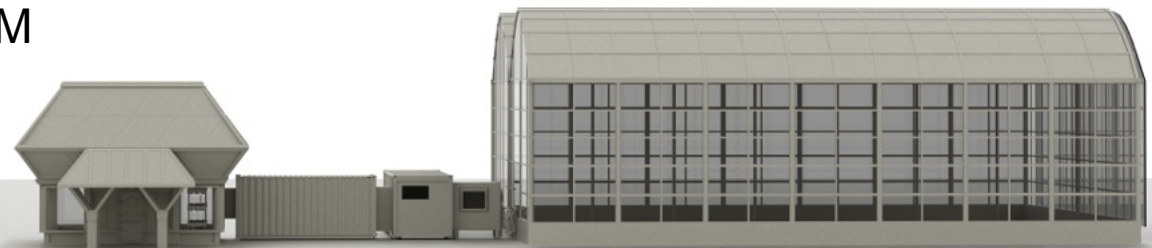
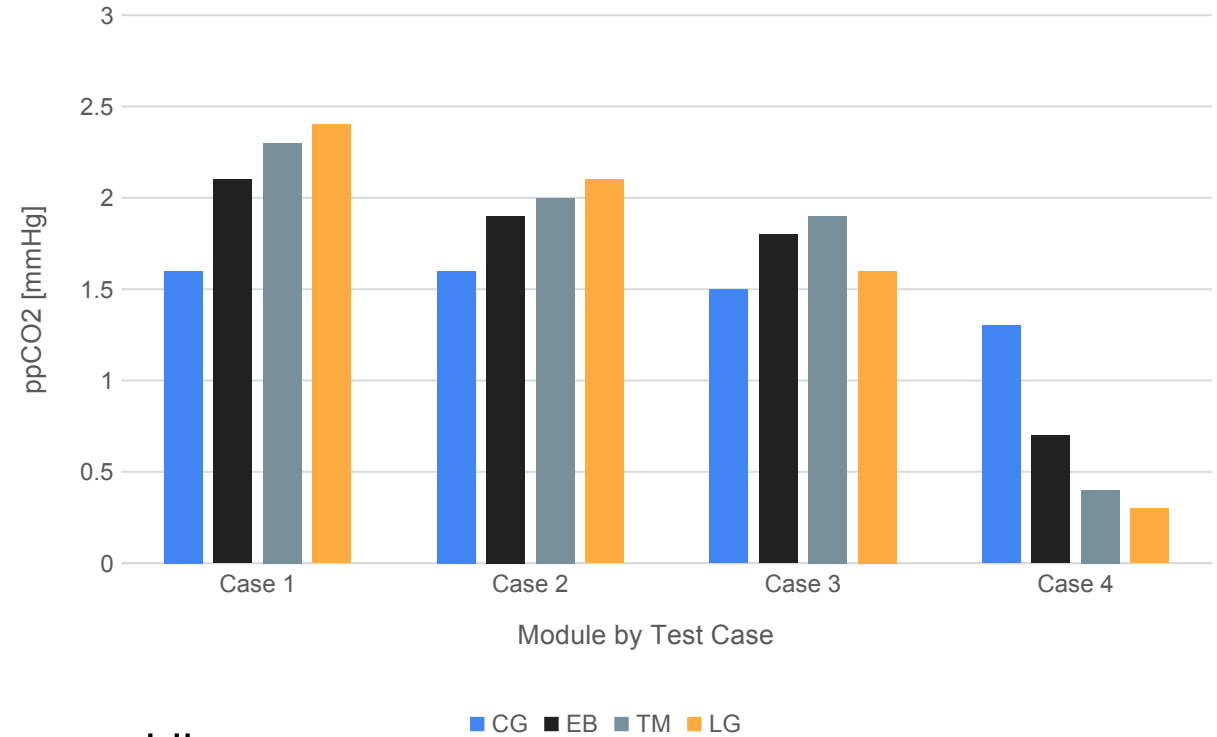


Summary of Conditions for Analysis Cases

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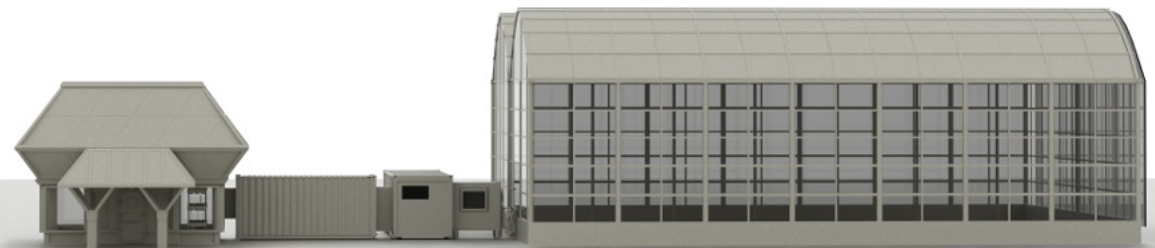
Key Conclusions

- Case 1 results in highest CO₂ levels
- Case 4 results in lowest CO₂ levels
- All cases remain in acceptable CO₂ range
- Case 3 selected as design configuration due to overriding design criteria:
 - CW airflow prevents humidity from TM into CQ
 - CW airflow provides CO₂ to plants in TM



Completed since the prior, 2025 paper

- Constructed the new Experimental Air Revitalization Laboratory (EARL)
 - An open air, separate structure from SAM
 - Includes internal power distribution, dedicated (oversized) room cooling, and a scrubber coolant loop
- Built the SAM Carbon Dioxide Removal Assembly (SCDRA - “skee-druh”)
 - Selected the 4BCO₂ architecture as the design foundation
 - Licensed the technology from NASA Marshall
 - Zeolite-based, regenerable system
 - Combination of commodity, off-the-shelf-components; and
 - Custom fabricated chambers and wall-mount rigging

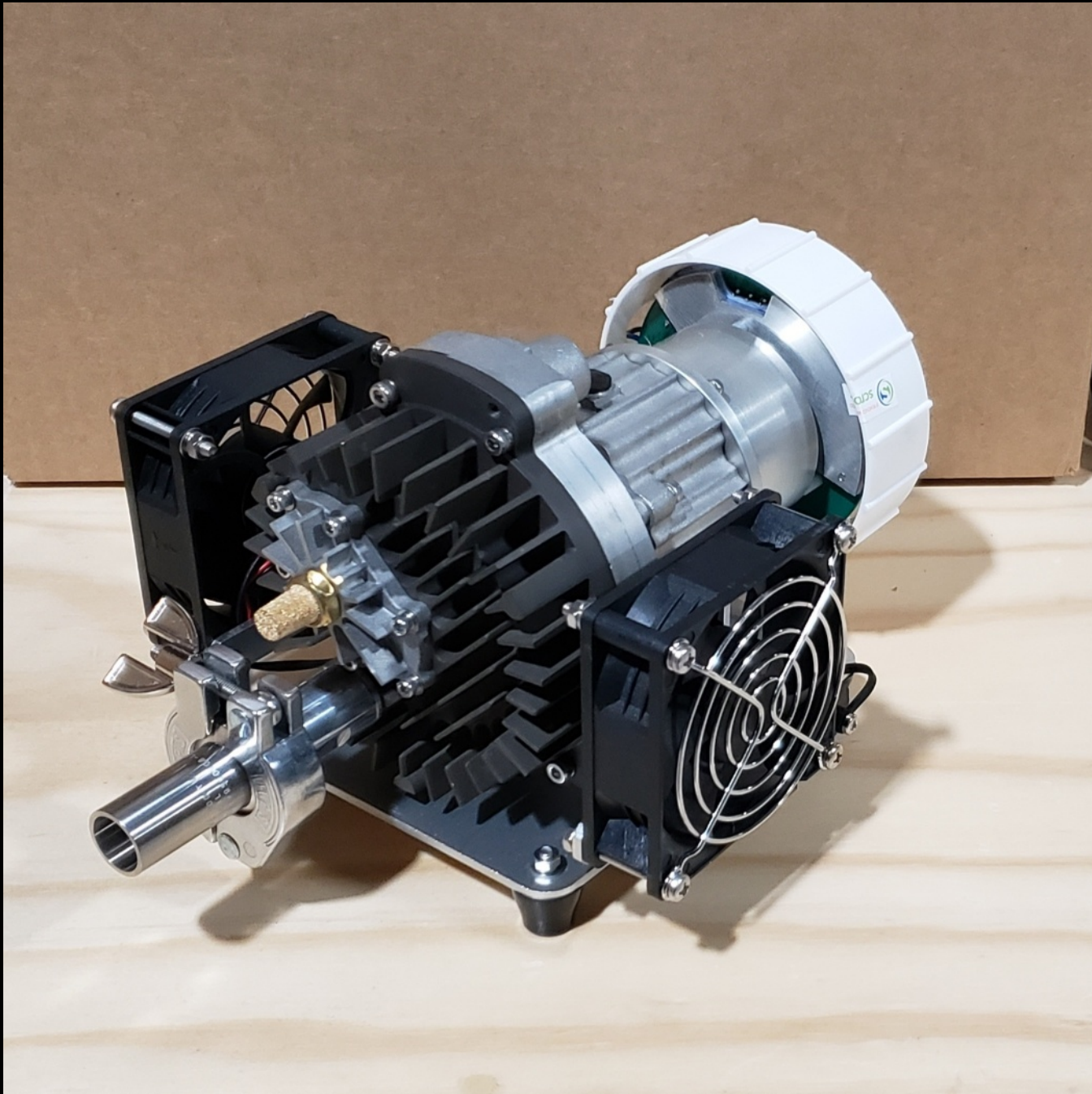




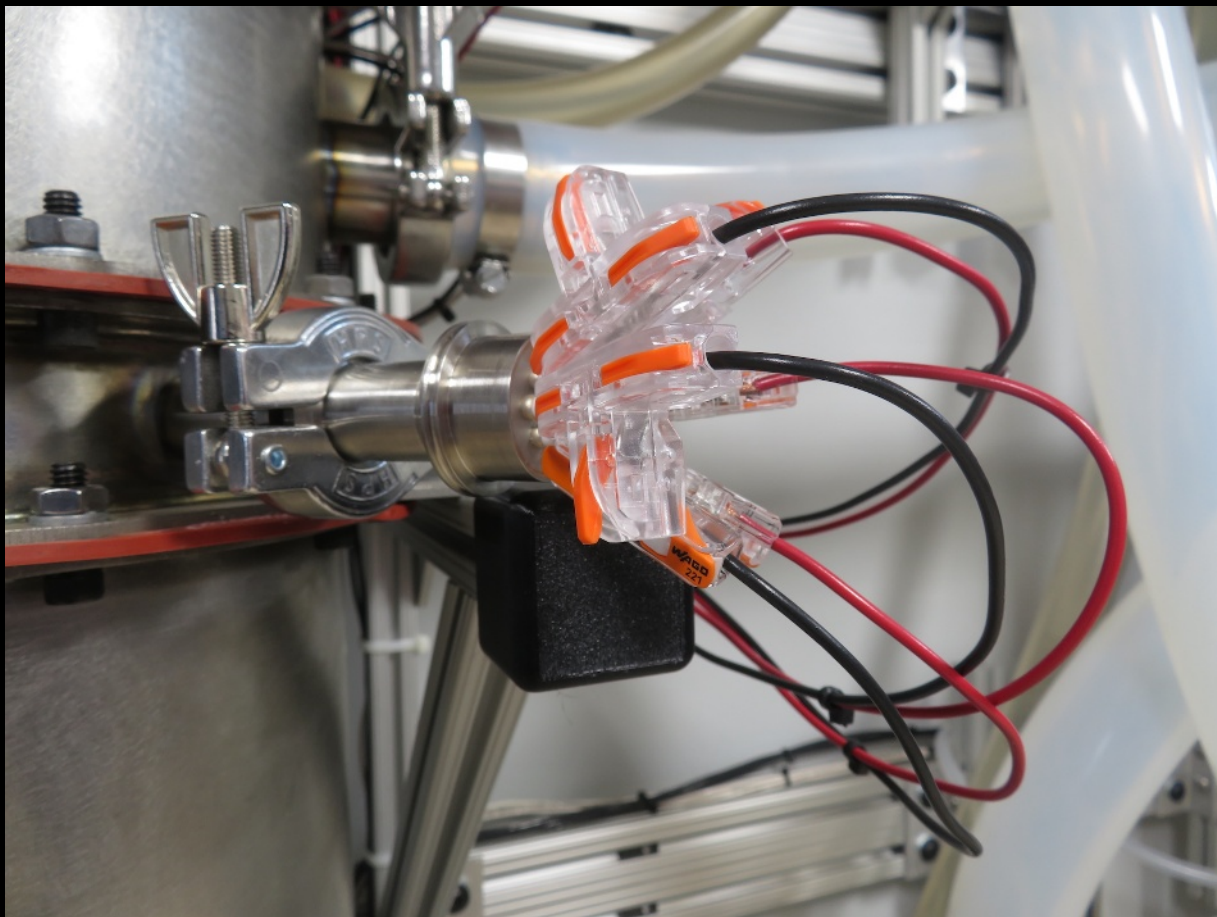


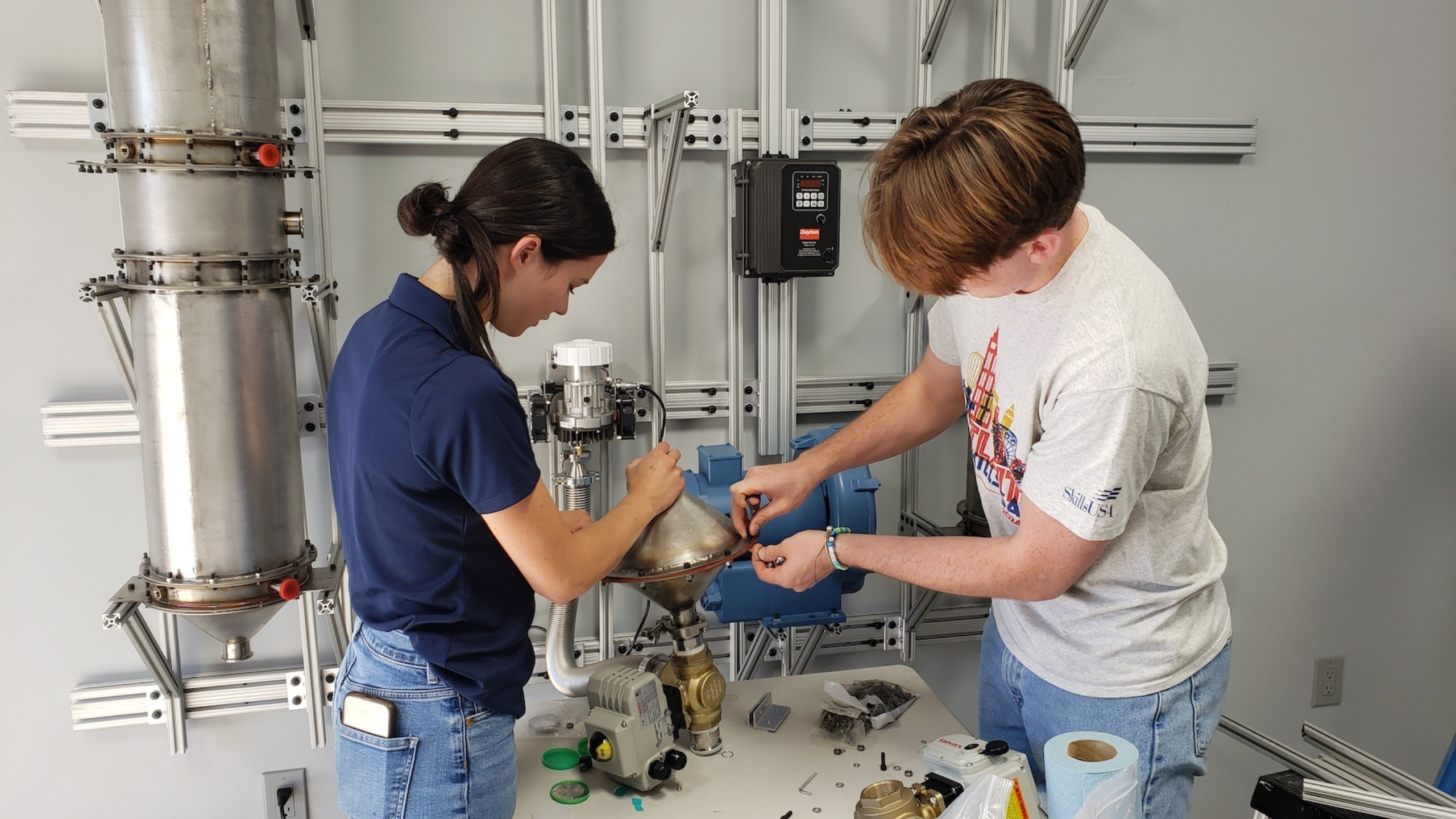






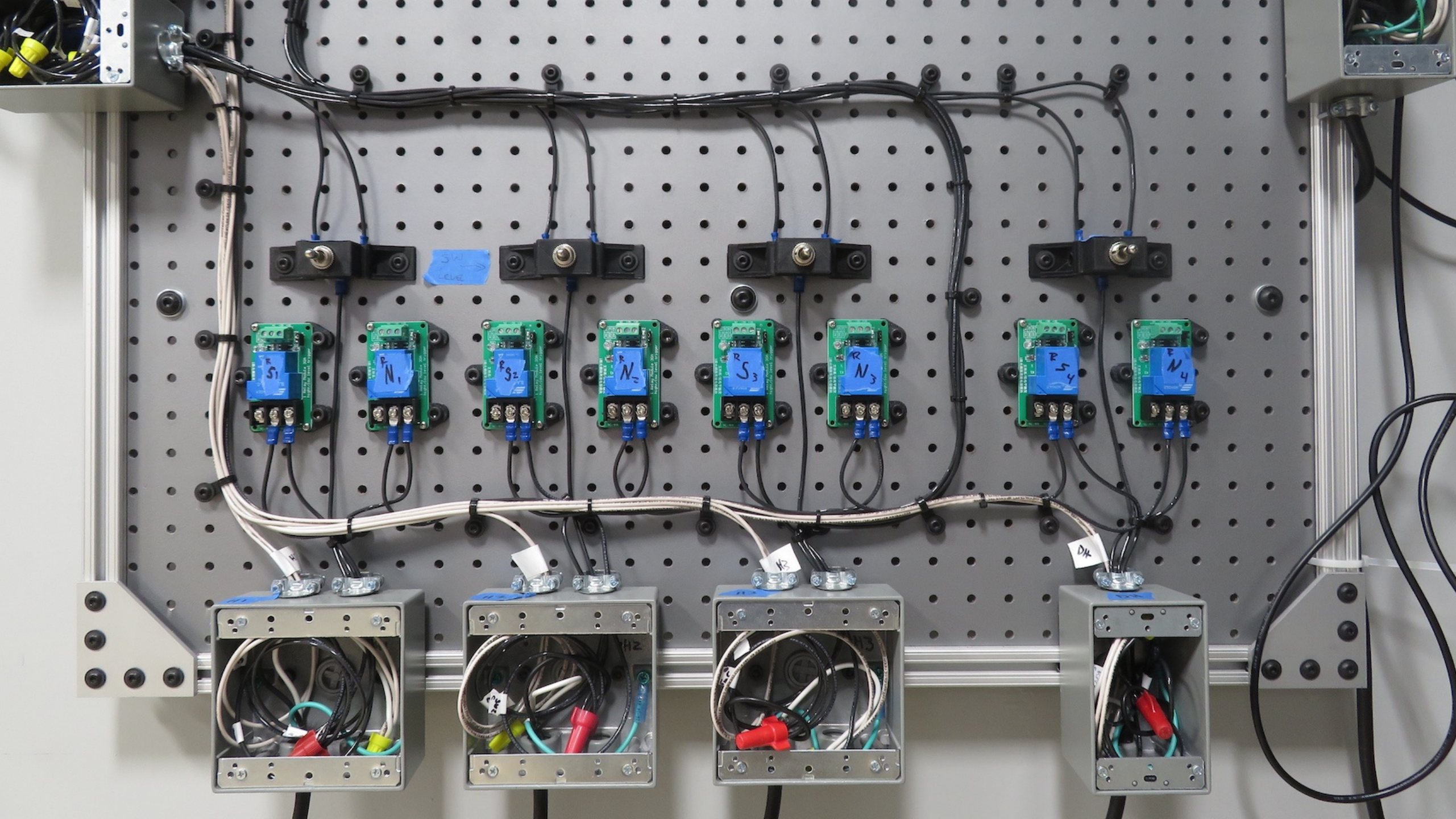






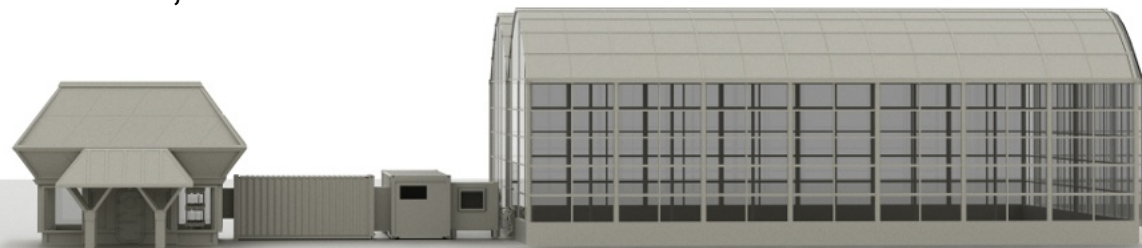
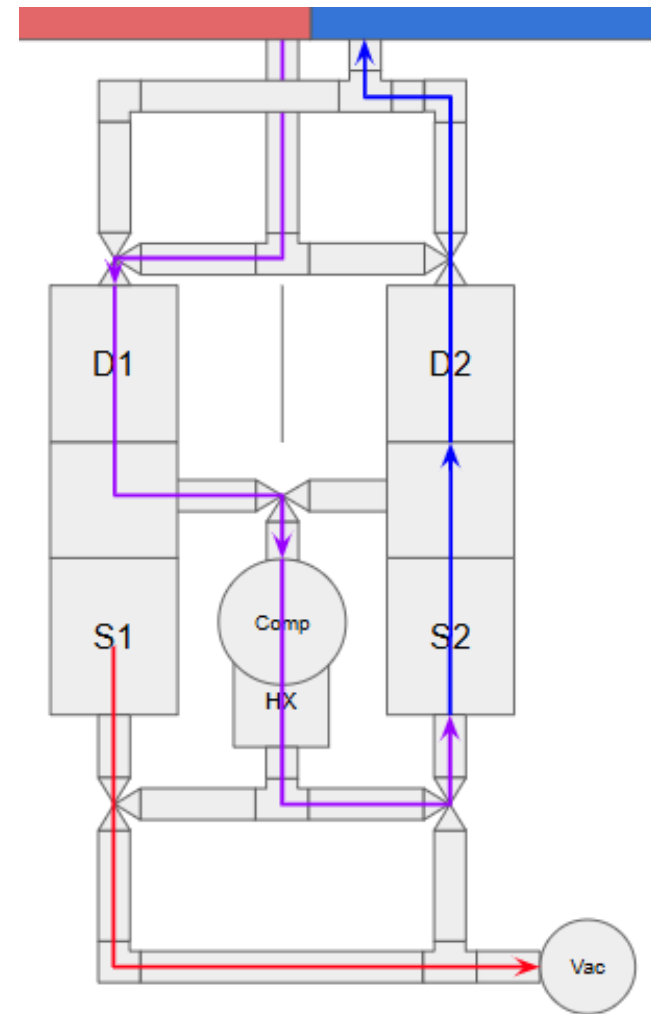






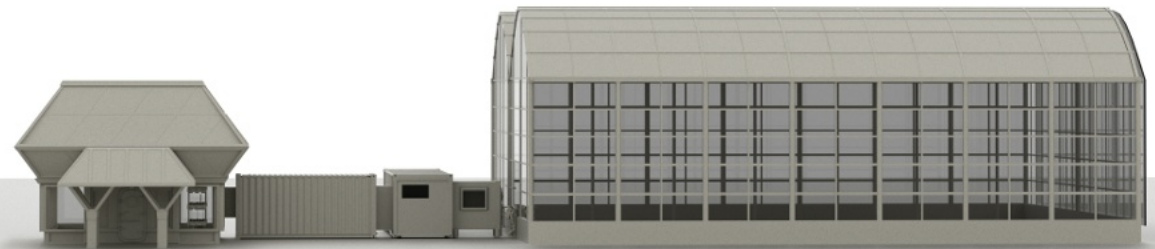
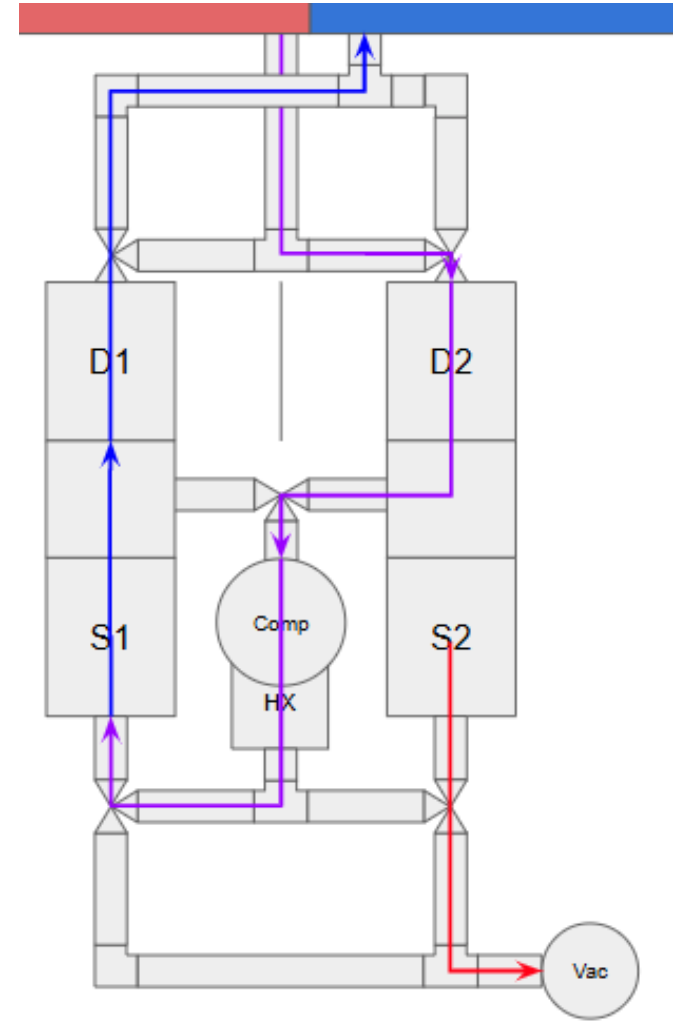
Air Flow for 1st Half Cycle

- 1) Air enters through a previously regenerated desiccant bed D1 where moisture from the air stream is removed.
- 2) Dehumidified air then enters the blower where it is pressurized.
- 3) The heat exchanger (HX) removes the heat of adsorption and compression, cooling the air to roughly 10°C (50°F).
- 4) CO₂ ladened, cool, dry air moves to sorbent bed S2, which is virtually devoid of CO₂ and hot at the beginning of this half cycle.
- 5) The in-bound air cools S2 such that it can adsorb again, and CO₂ is removed from the air stream.
- 6) As the start of this half cycle, the out-bound air is hot, and forces the moisture from desiccant bed D2 back into the airstream.
- 7) The air then leaves the system carrying the same total moisture as was input to the system over the previous half-cycle, but minimal CO₂.
- 8) Sorbent bed S1, loaded with CO₂, is isolated, exposed to vacuum (space on ISS; vacuum pump at SAM), and heated;
- 9) This desorbs the CO₂ through the exhaust line.



Air Flow for 2nd Half Cycle

- 1) The cycle then flips and each bed assumes the opposite role.
- 2) Airflow enters the freshly desorbed desiccant bed D2 and continues into the freshly desorbed sorbent bed S1.
- 3) Continues through the now-loaded desiccant bed D1, causing it to release its moisture; while
- 4) The loaded sorbent bed S2 is isolated and the CO₂ is desorbed to vacuum, and through the exhaust line.

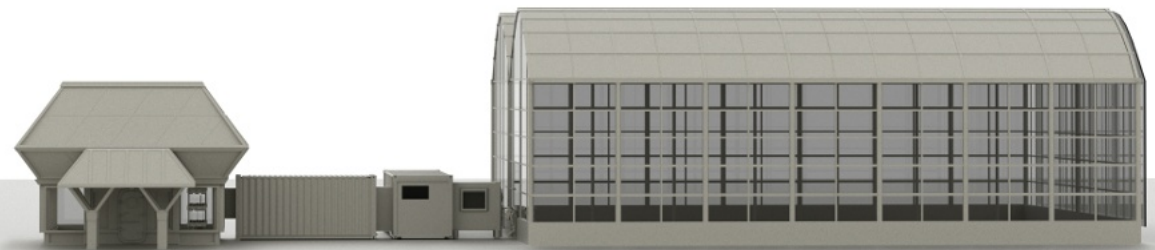


Half Cycle Test Procedure

- 1) Sealed front door to EARL to minimize air exchange. Rear door remained operable.
- 2) Set fan to circulate CO₂ upon injection from external canister.
- 3) Raised the CO₂ level to 5000 ppm.
- 4) Ran 30 minutes baseline for CO₂ loss. *
- 5) Ran #3-4 again, with human inside to account for additional CO₂. **
- 6) Injected CO₂ to 5000 ppm.
- 7) Ran adsorb half-cycle.
- 8) Ran desorb half-cycle.

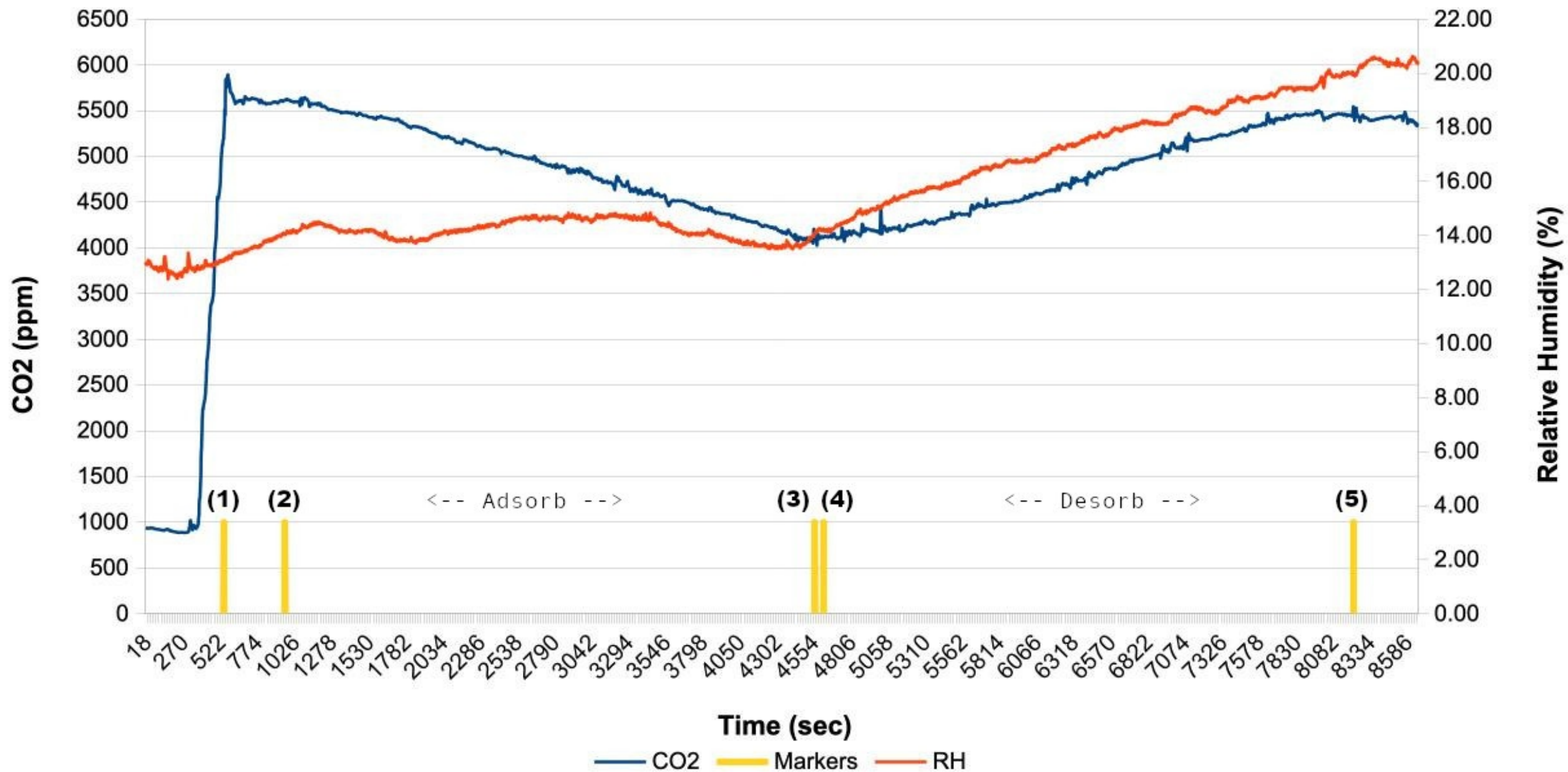
* SIMOC Live captured CO₂, relative humidity, and temperature.

** 2-way radios were used to monitor levels, coordinate CO₂ injection, cycle start and stop.





SAM EARL Scrubber - Half Cycle Test



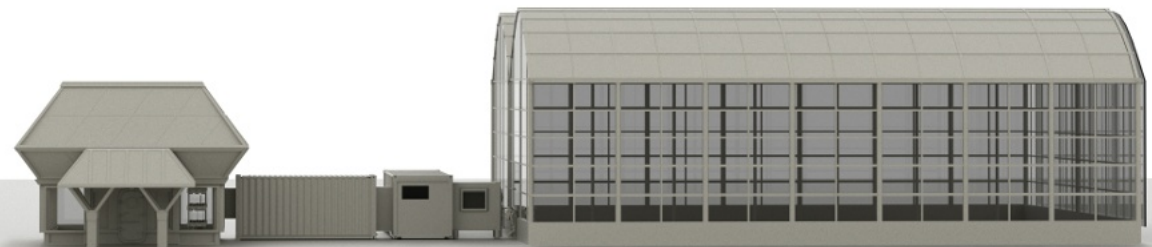
Half Cycle Test results



Adsorb			Desorb		
Initial CO ₂	Final CO ₂	Adsorption Rate	Initial CO ₂	Final CO ₂	Desorption Rate
5610 ppm	4150 ppm	1406 ppm/hr	4121 ppm	5493 ppm	1426 ppm/hr

CO ₂ Removal Rate Summary				
	Ppm CO ₂ / hr	Mol CO ₂ / (mol air * hr)	kg CO ₂ / hr	kg CO ₂ / day
Adsorb	1406	0.001406	0.167	4.01
Desorb	1426	0.001426	0.170	4.08

- Operated at 5000 ppm CO₂
- Target removal rate was 4.5 kg/day
- Actual removal rate was 4.01 kg/day
- Reasons for shortfall:
 - Incomplete desorb of desiccant bed
 - Incomplete desorb of sorbent bed
 - Lower flow rate than nominal (designed for 25 cfm; run at 22.3)



Thank You!

Questions?

Kai Staats, MSc
kai@overthesun.com

Dr. James Knox
james.knox.mail@gmail.com

www.moonandmars.space

